- 5. I. N. Frantsevich, in: High-Accuracy Electrical Contacts [in Russian], Naukova Dumka, Kiev (1970).
- 6. B. A. Marek and V. S. Chemeras, in: High-Accuracy Electrical Contacts [in Russian], Izd. Akad. UkrSSR, Nauk, Kiev (1972).
- 7. P. I. Zaitsev, I. G. Nekrashevich, and A. V. Smirnov, in: High-Accuracy Electrical Contacts [in Russian], Izd. Akad. Nauk UkrSSR, Kiev (1972).
- 8. H. S. Carslaw and J. C. Jaeger, Conduction of Heat in Solids, Oxford University Press (1959).
- 9. L. I. Rubinshtein, Stefan's Problem [in Russian], Zaigzne, Riga (1967).
- 10. G. E. Gorelik, N. V. Pavlyukevich, T. L. Perel'man, and G. I. Rudin, Inzh.-Fiz. Zh., 24, No. 3, 525 (1973).
- 11. R. Holm and E. Holm, Electric Contacts: Theory and Application, Springer-Verlag (1967).

HEAT EXCHANGE IN THERMALLY INITIAL PORTION OF TUBE WITH VARIABLE WALL TEMPERATURE

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An asymptotic solution is obtained for the laminar heat-exchange problem with variable wall temperature.

The heat problem for the boundary layer on the surface whose temperature follows the law

$$T_w = T_0 + Ax^{\gamma}, \tag{1}$$

possesses a self-similar solution; it was studied in detail in [1] primarily by asymptotic methods.

The thermally initial portion of the tube where the liquid temperature varies from its value at the wall T_W to the temperature of the flow core, T_0 , is equal to the incoming temperature; this takes place in the region $\delta \ll d$ (see Fig. 1), and can be analyzed in the same way as a boundary layer; the self-similar solution of the heat problem can also be obtained.

In the case of $T_w = \text{const} [\gamma = 0 \text{ in (1)}]$ this solution was obtained first by Leveque [2]. Attempts to generalize this solution to the variable case were made by Leveque himself [2] and also by others in [3, 4] although Nu as a function of γ was not available as is the case in a boundary-layer problem.

In the present article the Leveque solution is directly generalized to the case of the wall temperature following a power law.

The heat equation for the thermally initial portion is given by [5]

$$\rho c_p u \frac{\partial T}{\partial x} = \lambda \frac{\partial^2 T}{\partial y^2}. \tag{2}$$

In a thin heat-exchange layer the liquid velocity can be regarded as proportional to y:

$$u = \beta y. \tag{3}$$

In particular, for laminar flow in a circular tube one has [5]

$$\beta = 8\overline{u}/d. \tag{4}$$

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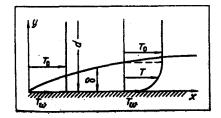


Fig. 1. Heat-exchange diagram in the thermally initial portion.

Equation (2) must be solved under the conditions

$$T = T_w$$
 for $y = 0$,
 $T \to T_0$ for $y \to \infty$. (5)

Adopting (1) for $T_{\mathbf{W}}$ we now introduce the dimensionless temperature

$$\theta = \frac{T - T_0}{T_{10} - T_0} \tag{6}$$

and the Leveque similarity variable [5]

$$\eta = (9\kappa x)^{-1/3} y, \tag{7}$$

where

$$\kappa = \lambda/(\beta \rho c_p). \tag{8}$$

Then (2) becomes an ordinary differential equation (primes denoting differentiation with respect to η)

$$\theta'' + 3\eta^2\theta' - 9\eta\eta\theta = 0. \tag{9}$$

The conditions (5) now become

$$\theta = 1 \text{ for } \eta = 0, \quad \theta \to 0 \text{ for } \eta \to \infty.$$
 (10)

Equation (9) is a particular case of the equation

$$\theta'' + a\eta^2\theta' + b\eta\theta = 0$$

for

$$a=3, \quad b=-9\gamma, \tag{11}$$

which under the conditions (10) yields [6]

$$-\theta'(0) = \frac{\Gamma\left(\frac{2}{3}\right)\Gamma\left(1-\frac{b}{3a}\right)}{\Gamma\left(\frac{4}{3}\right)\Gamma\left(\frac{2}{3}-\frac{b}{3a}\right)} \left(\frac{a}{3}\right)^{\frac{1}{3}}.$$
 (12)

Substituting (11) into (12) one obtains

$$-\theta'(0) = \frac{\Gamma\left(\frac{2}{3}\right)\Gamma(1+\gamma)}{\Gamma\left(\frac{4}{3}\right)\Gamma\left(\frac{2}{3}+\gamma\right)}.$$
 (13)

It follows from (1), (6), and (7) that

$$\left(\frac{\partial T}{\partial y}\right)_{y=0} = \frac{Ax^{\gamma-\frac{1}{3}}}{(9x)^{1/3}} \theta'(0). \tag{14}$$

Introducing the Péclet number,

$$Pe = \frac{\overline{ud\rho c_p}}{\lambda},\tag{15}$$

and the local Nusselt number,

$$Nu = \frac{-(\partial T/\partial y)_{y=0} d}{T_w - T_0}$$
 (16)

and with the aid of (4), (8), and (13)-(15), one obtains

$$Nu = \frac{2\Gamma\left(\frac{2}{3}\right)\Gamma(1+\gamma)}{9^{1/3}\Gamma\left(\frac{4}{3}\right)\Gamma\left(\frac{2}{3}+\gamma\right)} \left(Pe^{\frac{d}{x}}\right)^{\frac{1}{3}}.$$
 (17)

The formula (17) expresses the Nusselt number for a laminar flow in the thermally initial portion of a circular tube with the wall temperature following the law (1).

In the particular cases either of $\gamma = 0$ (wall temperature remains constant), or of $\gamma = 1/3$ (constant flow), or $\gamma = 1$ (wall temperature changing linearly) the results which follow from the formula (17) are the same as those obtained in [3, 4] by employing a different approach.

For $\gamma = 0$ the formula (17) yields the Leveque solution [5]

$$Nu = 1.077 \left(Pe \frac{d}{x} \right)^{\frac{1}{3}}.$$

It is noted that in view of the assumption (3) and the form of Eq. (2) the solution (17) is an asymptotic one and becomes valid for $[Pe(d/x)] \gg 1$ [5].

NOTATION

T, temperature of liquid; T_W , wall temperature; T_0 , incoming temperature; A, γ , constants [formula (1)]; x, lengthwise coordinate; y, transverse coordinate; δ , thickness of thermal boundary layer; ρ , liquid density; c_p , specific heat; λ , thermal conductivity; u, velocity; u, mean velocity; e_p , Péclet number; e_p , Nu, local Nusselt number.

LITERATURE CITED

- 1. I. Imai, Quart. Appl. Math. 16, No. 1 (1958).
- 2. M. Leveque, Ann. Mines, 13, No. 4 (1928).
- 3. W. M. Kays, Trans. ASME, <u>77</u>, No. 8 (1955).
- 4. J. R. Sellar, M. Tribus, and J. S. Klein, Trans. ASME, 78, No. 2 (1956).
- 5. B. S. Petukhov, Heat-Exchange and Resistance for Laminar Flow of Liquids in Tubes [in Russian], Énergiya, Moscow (1967).
- 6. S. L. Lur'e, Izv. Vyssh. Uchebn. Zaved., Energet., No. 6 (1968).